

~~MAKAROV~~ ~~Vladimir Ivanovich~~, kandidat tekhnicheskikh nauk; FEYNBERG, G.M.,
inzhener, nauchnyy redaktor; BURMISTROV, G.N., redaktor; KUZ'MIN,
D.G., tekhnicheskiiy redaktor

[Operator of road machinery] Motorist dorozhnykh mashin. Moskva,
Vses.uchebno-pedagog. izd-vo Trudrezervizdat, 1956. 351 p.
(Road machinery) (MIRA 10:2)

BOGUSHEVSKIY, A.A., kand.tekhn.nauk, GALIYAMIN, Ye.P., inzh.,
ZENCHENKO, A.A., inzh., MAKAROV, V.I., inzh.

Land reclamation for agricultural use in the Yakut A.S.S.R. Gidr.
1 mel. 12 no.8:3-9 Ag '60. (MIRA 13:8)
(Yakutia--Irrigation) (Yakutia--Drainage)

MAKAROV, Vladimir Genadiyevich; ASTASHKEVICH, Ye.T., ekonomist, retsenzent;
BOCHAROV, G.G., ekonomist, red.; TKACHUN, A.I., red. izd-va; MODEL,
B.I., tekhn. red.

[Accounting theory; accounting principles in industry] Teoriia
bukhgalterskogo ucheta; osnovy teorii bukhgalterskogo ucheta v
promyshlennosti. Moskva, Gos. nauchno-tekhn. izd-vo mashino-
stroit. lit-ry, 1960. 159 p. (MIRA 14:9)

(Accounting)

MAKAROV, V.G.

Combined flowsheet for the production of forgings. Kuz.-shtam.
proizv. 3 no.7:44-46 JI '61. (MIRA 14:6)
(Forging) (Industrial organization)

MAKAROV, V.G.

Forging of duralumin pistons. Kuz.-shtam. proizv. 3 no.1:47-48
Ja '61. (MIRA 14:1)
(Forging) (Duralumin)

MAKAROV, V.G.; FINKEL', S.M.; SHESTAKOV, K.T.; STARCHAKOVA, I.I.,
red.; KISELEVA, A.A., tekhn.red.

[Accounting in state commerce] Bukhgalterskii uchet v gosudarstvennoi torgovle. Moskva, Gos.izd-vo torg.lit-ry, 1960.
252 p. (MIRA 14:3)

(Accounting)

VASIL'YEV, Yu.V.; MAKAROV, V.G.; POGOSOV, Yu.L.

Methods of manufacturing laboratory apparatus and equipment
of polyethylene. Zashch. 38 no. 4:507-508 '62. (MIRA 15-3)

J. Moskovskiy tekstil'nyy Institut i Institut khimii polimero
AN USSR.

(Laboratories: Equipment and supplies)
(Polyethylene)

FROLOV, I.A.; MAKAROV, V.G., elektromekhanik

Magnetic recording head polishing device. Avtom., telem. i sviaz' 2
no.3:23-24 Mr '58. (MIRA 13:1)

1. Starshiy elektromekhanik Moskovskoy distantstii signalizatsii i svyazi
Moskovsko-Kursko-Donbasskoy dorogi (for Frolov).
(Magnetic recorders and recording)

MAKAROV, V.G.; RUDENCHIK, A.A.

Enlarged work teams for track sections. Put' i put. khoz. no.7:
18-19 J1 '57. (MLRA 10:8)

1. Nachal'nik Vspol'inskoy distantzii, stantsiya Vspol'ye (for
Makarov). 2. Zamestitel' nachal'nika Vspol'inskoy distantzii, st.
Vspol'ye (for Rudenchik).
(Railroads--Management)

MAKAROV, V. G., Cand Agr Sci -- "Socialist agriculture ^{transformation} ~~trans-~~
~~formation~~ of the Komi ASSR far north.) (^{livestock raising} ~~Cattle~~-breeding,
reindeer ^{raising} ~~breeding~~, and wild-animal ^{hunting} ~~breeding~~ on Izma)."
Mos, 1961. (All-Union Agr Inst of Correspond^{ing} Ed) (KL, 8-61,
254)

KOMLEV, G.A.; KLEANDROV, T.N.; CHAKHOTIN, V.S.; UDALOV, L.R.; MAKAROV, V.F.

Reducing losses of metal in the processing of mercury ores in rotary tube furnaces. Izv.AN Uz.SSR.Ser.tekh.nauk 8 no.4:66-69 '64.
(MIRA 18:4)

1. Sredneaziatskiy filial Gosudarstvennogo nauchno-issledovatel'skogo instituta tavetnykh metallov.

ACC NR: AT6036427

finding was that the rate of exoelectron emission from the surface of a metal is influenced by and commensurate with the degree of the metal's previous cold deformation. Thus the counting rate for specimens of sheet aluminum deformed 50% is roughly four times as high (20 pulses/sec) as the counting rate for specimens deformed 10% (~5 pulses/sec). It is thus clear that the exoelectron emission method represents a major new technique of metallographic investigation. Orig. art. has: 11 figures.

SUB CODE: // / SUBM DATE: none/ ORIG REF: 001/ OTH REF: 002

Card 4/4

ACC NR: AT6036427

The investigation was performed with the aid of a setup specially designed and constructed in the Moscow Institute of Aviation Technology and consisting of a SI-2B gas-discharge counter, a PS-10000 scaler, an ISS-3 counting rate meter, a tank for the preparation of the quenching mixture and a KhA thermocouple for measuring the specimen's temperature. The setup is equipped with a furnace for heating specimens to a temperature of 300°C. Findings: with heating of the specimen the number of pulses monotonically increased. On slow cooling of the specimen an emission peak corresponding to the crystallization temperature was recorded. In general, the very presence of an emission peak makes it possible to determine the temperature of phase transformations. With respect to Sn alloys the emission peaks at the instants of phase transformation were 22, 32 and 42 pulses/sec, respectively, which is in good agreement with theory (constitution diagram of Sn-Pb) and the experimental findings of Futschik et al. (Z. Physik, H. 145, Nr. 48, 1956). New experimental findings were obtained on the exoelectron emission of alloys of the Al-Zn system. In particular, the investigation of exoelectron emission in the presence of solid-state transformations of alloys with 8 and 15% Zn established complete correspondence between the position of emission peaks on the temperature axis with the line of limited solubility of Zn in Al in solid state. Further, it is established that the magnitude of the emission peak is independent of the thermal effects of the transformations. Hence the exoelectron emission method serves equally well to determine both the transformations from liquid to solid state and from solid to liquid state. Another new

Card 3/4

ACC NR: AT6086427

investigated. Specimens 1-2 mm thick and measuring from 20 to 250 mm² in area were placed on a mica sheet atop a hollow water-cooled steel base plate (Fig. 1).

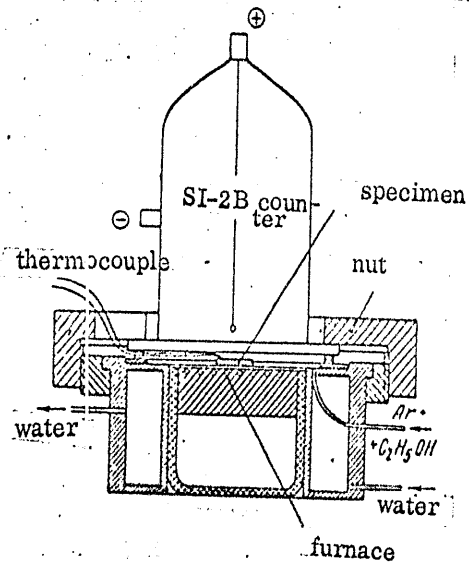


Fig. 1. Schematic representation of the design of the base plate for a Geiger-Mueller counter

ACC NR: AT6036427

SOURCE CODE: UR/2536/66/000/066/0174/0182

AUTHOR: Rostovtsev, G. N. (Candidate of technical sciences); Makarov, V. D. (Engineer)

ORG: none

TITLE: Investigation of phase and structural transformations in metals and alloys with the aid of exoelectron emission

SOURCE: Moscow. Aviatsionnyy tekhnologicheskii institut. Trudy, no. 66, 1966. Struktura i svoystva aviatsionnykh staley i splavov (Structure and properties of aircraft steels and alloys), 174-182

TOPIC TAGS: *ALLOY PHASE DIAGRAM;* gas discharge counter, scaler, count rate meter, exoelectron emission, electron emission, metal surface, tin, aluminum base alloy, phase composition / SI-2B gas discharge counter, PS-1000 scaler, ISS-3 count rate meter

ABSTRACT: The purpose of this project was to develop methods of investigating phase and structural transformations by means of exoelectron emission on using modern electronic apparatus. Tin, alloys of tin with lead (14, 38.1 and 94% Pb), alloys of aluminum with zinc (8 and 15% Zn), and sheet aluminum subjected to various degrees of deformation were thus in-

Card 1/4

UDC: 669.017:620.18

MAKAROV, V.D.

Characteristics of mining the lower levels of the Verkhniy Zgid
deposit. Gor. zhur. no.4:27-29 Ap '65. (MIRA 18:5)

1. Glavnyy inzh. Sadonskogo rudoupravleniya.

MAKAROV, V.D.

More productive variants in the system of working thin veins with shrinkage stoping with backfill. Gor. zhur. no.5:29-31 My '63.
(MIRA 16:5)

1. Glavnyy inzh. Sadonskogo rudoupravleniya.
(Sadon region--Mining engineering)

AKIF'YEV, A.P.; MAKAROV, V.B.; POLUNOVSKIY, V.A.; YURCHENKO, V.V.

Study of chemical mutagenesis in a transplanted culture of
L-cells. Genetika no.3:19-26 3 '65.

(MIRA 18:12)

1. 2-y Moskovskiy meditsinskiy institut. Submitted June 12,
1965.

MAKAROV, V.B., inzh. (g.Kuybyshev)

Precast paving of the earth slopes of hydraulic structures with
reverse filters from porous concrete. Gidr. 1 mel. 12 no.10124-29
(MIRA 13:11)

Q '60.

(Hydraulic structures)

(Precast concrete construction)

KOLOTYRKIN, Ya.M.; MAKAROV, V.A.; KUZUB, V.S.; TSINMAN, A.I.; KUZUB, L.G.

Anodic protection of heat exchangers made of 1Kh18N9T steel in concentrated sulfuric acid at temperatures of 100 - 120°. Zashch. met. 1 no.5:598-600 S-O '65. (MIRA 18:9)

1. Nauchno-issledovatel'skiy fiziko-khimicheskiy institut imeni L.Ma.Karpova, Moskva.

26105-05
ACCESSION NR: AP4047015

Enlargement of the particle size produces no increase in strength. As shown in Fig. 2 of the Enclosure, however, the strength of a welded spot is less when coarse powder is used. The effect of the density of the powder layer was investigated on aluminum specimens for iron powder 100 - 180 μ in diameter. The specimens were also tested for sensitivity to impurities. As shown in Fig. 3 of the Enclosure, the presence of a non-metal on the surface somewhat reduced the strength of the weld. The authors concluded that the dimensions of the powder should be no less than 150 - 200 microns; the density of the layer of powder should be approximately 0.5 mm; and the relative depth of the punch impressions should be 70 - 75% for aluminum and 85-87% for copper (not taking into account the density of the layer of powder). Orig. art. has: 1 table and 7 figures.

ASSOCIATION: Institut avtomatskoi i mekhaniki AN Latvyskoy SSR (Automation and Mechanics Institute, AN Latvian SSR)

EXEMPTED: 00

ENCL: 03

HUB CODE: MM

NO REL SOV: 00

OTHER: 00

26105-45 EMP(a)/EMP(m)/EMP(v)/I/ERR/EMP(c)/EMP(k)/EMP(b) PF-1/Ps-1 LJP(c)
 REGISTRATION NR: AP404/015 JD/HM S/0135/84/009/010/0028/0031

AUTHOR: Avbinder, S. B. (Candidate of technical sciences); Loginova, A. Ya. (Engineer);
 Makarov, V. A. (Engineer); Rastrigina, E. F. (Candidate of technical sciences)

TITLE: Cold welding of metals using solid finely divided particles

SOURCE: Svarochnye proizvodstvo, no. 10, 1964, 28-31

TOPIC TAGS: cold welding, spot welding, metal treatment, metal impurity, metal powder,
 aluminum base alloy, aluminum welding, copper welding

ABSTRACT: This article presents the results of investigations concerning the development
 of a method of cold spot welding which does not require special surface treatment of the
 metal and which is relatively insensitive to impurities. A layer of iron, sand, emery,
 nickel, or aluminum powder was applied to the surface of aluminum and copper specimens
 3x30x60 mm in dimensions. It was determined from these tests that the powder must be
 harder than the specimens being welded, and that powder from reduced iron produced the
 best results. The effect of the particle size of the powders was also investigated. As
 shown in Fig. 1 of the Enclosure, increasing the dimensions of the powder particles in-
 creases the strength of the welded spot to a certain limit, after which subsequent en-

and 1/5

L 18595-65

ACCESSION NR: AP-007109

1. Design parameters for the guides determined by calculation. When the pressure in the collector was 4 atmospheres, the air consumption with a nozzle diameter of 0.5 mm was 9.2 m³/h and with a diameter of 0.3 mm was 3.2 m³/h. The operation of the system was practically noiseless. Orig. art. has 5 figures, 5 graphs.

ASSOCIATION: none

SUBMITTED: 00

ENG: 00

SUB CODE: IE, ME

NO REF SOV: 000

OTHER: 000

JPRS

Card 1/4

1. 18597-65
ACCESSION NO. AP500375

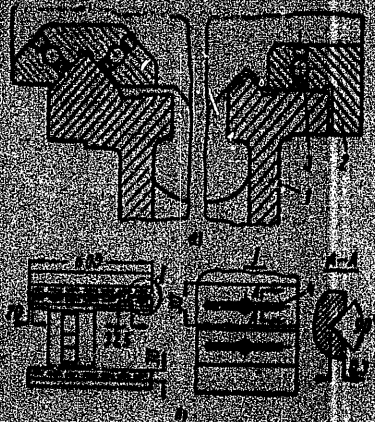
0

Drilled through the body of the carriage 2 are air channels through which air is fed to nozzles 3. From the aperture of the nozzles, the air goes into pocket 4 which is made in the form of a groove along the axis of the guide. This type of pocket forms a plane-parallel stream of air which flows from the pocket into the gap between carriage 2 and bed 1. The LA67-2.5 brass nozzle is pressed into the aperture in the carriage and scraped flush with the surface of the guide. The height of buoyancy was measured at six points (three on prismatic and three on flat guides). The arithmetical average of measurements at three points for each guide is taken as the height of buoyancy. The carriage was loaded by two tuning fork dynamometers (directly over the guides) until the gap for both guides was less than 3 microns. At this point the loading (taking the weight of the carriage into account) was: 1) for a nozzle diameter of 0.2 mm at a pressure in the collector of 4 atmospheres, 282 kg; at 3 atmospheres, 237 kg; 2) for a nozzle diameter of 0.5 mm at a collector pressure of 4 atmospheres, 311 kg; at 3 atmospheres, 270 kg. The average value of the rigidity for both guides with a gap of 3 microns and a pressure of 4 atmospheres was: 12 kg/micron when the nozzle diameter was 0.2 mm; 9 kg/micron when the nozzle diameter was 0.5 mm. It should be noted that the rigidity of even such narrow guides as those on the stand may be raised still more by more ration-

Card 3/4

1 18595-05
 NO. 18595-05

carriage was 80h 15-32 cast iron, for the bed--MSCh 28-48 cast iron. The design of the aerostatic guides is shown schematically in the drawing below.



Design of aerostatic guides: from the side of the guides
 a) section through the nozzles; b) carriage

10095-65

ACCESSION NO. AF0005105

8/0121/8-000/009/0010/0013

AUTHOR: Makarov, V. A.

TITLE: Experimental study of the dynamic characteristics of aerostatic guides

SOURCE: Stand. i Instrument, no. 9, 1964, 10-15

TOPIC TAGS: machine tool; lathe

Abstract: One of the means for raising the accuracy of displacement of the working units of precision machine tools is to create an aerostatic cushion for the guides. This study was conducted in order to clear up the character of the amplitude-frequency characteristics of aerostatic guides in relationship to the damping force and the point of its application and to determine ways for reducing the amplitude of degenerate oscillations. The work was conducted by Mostankin (Moscow Machine Tools and Instruments) in the machine tool laboratory of the Krasny Proletariy factory. The study was conducted on a stand set up on the base of a model 1K62 screw cutting lathe. The aerostatic cushion was created between the guides of the bed and the carriage. The guides for the bed were ground (7th class surface finish) those for the carriage were scraped (10-12 spots in a square with a side of 25 mm). The material for the

Card 1/4

SHTEYNBERG, D.S.; FOMINYKH, V.G.; MAKAROV, V.A.

Composition of pyroxenes in the Kachkanar intrusive complex.
Trudy Inst. geol. UFAN SSSR no.70:56-57 1965. (MIRA 18:12)

IPATENKO, N.G.; NESTEROV, T.S., dotsent; KUTILOV, I.N., dotsent; AKOPYAN, Ye.Sh.,
kand.veterin.nauk; KARAVAYEV, V.M.; PENIONZHKO, A.M.; MAKAROV, V.A.,
assistent.

Veterinary sanitation expertise. Veterinariia 41 no.3:83-93 Mr '64.
(MIRA 18:1)

1. Unravleniye tsentra Ministerstva proizvodstva i zagotovok sel'sko-
khozyaystvennykh produktov RSFSR (for Ipatenko). 2. Vitebskiy veterin-
rnyy institut (for Nesterov, Kutilov). 3. Vsesoyuznyy nauchno-issledova-
tel'skiy institut veterinarnoy sanitarii (for Akopyan). 4. Moskovskaya
veterinarnaya akademiya (for Makarov).

MAKAROV, V.A.

Our friends speak. Veterinariia 38 no.1:13-14 Ja '61.
(MIRA 15:4)

(Russia--Relations (General) with Bulgaria)
(Bulgaria--Relations (General) with Russia)

SHVERNIK, Aleksandr Mikhaylovich; SOKOLOV, Anatoliy Valentinovich;
 POLUBELOV, Aleksey Sergeyevich; KISELEV, Georgiy Ivanovich;
 BERNSHTEYN, Rafail Lazarevich; SLAVUTSKIY, Samuil Oskarovich;
 NEVEL'SHTEYN, Yuriy Grigor'yevich; KONDRATENKO, Leonid
 Fedorovich; LASKIN, Anatoliy Aronovich; LUR'YE, Zakhar
 Solomonovich; MAKAROV, Vladimir Aleksandrovich; NOVOZHILOV,
 M.G., retsenzent; BILLICHENKO, N.Ya., retsenzent; VARSJAVSKIY,
 A.M., retsenzent; TARTAKOVSKIY, B.N., retsenzent. Prinimali
 uchastie: ANTONOV, V.A., inzh.; VERBLYUNSKIY, Yu.I., inzh.;
 ZEMSKOV, P.F., otv. red.

[Overall mechanization and automatic control in strip mines]
 Kompleksnaya mekhanizatsiya i avtomatizatsiya na kar'erakh.
 Moskva, Nedra, 1964. 582 p. (MIRA 18:4)

MAKAROV, V.A.; MYACHIN, V.F.

Transistorized measuring equipment for marine automatic control
systems of the electrochemical protection against corrosion.
Inform. sbor. TSNIIMF no.64. Tekh. ekspl. mor. flota no.9:54-63
'61. (MIRA 16:6)

(Hulls (Naval architecture)--Corrosion)
(Cathodic protection)
(Automatic control)

SHAPOSHNIKOV, N.F., inzh.; MAKAROV, V.A., inzh.

Automation of the continuous flow-line concreting of the
Krasnoyarsk Hydroelectric Power Station. Mekh.stroi. 17
no.8:10-14 Ag '60. (MIRA 13:8)
(Krasnoyarsk Hydroelectric Power Station)
(Automatic control)

MAKAROV, V.A.

Source: KGB Archives, Moscow, Russia

Experimental investigation of dynamic characteristics of aerodynamic
guides, Stan.i Instr. 35 no.9:10-13 S 162. (MIRA 17:10)

MAKAROV, V. A.

~~Calculation of aerostatic guides.~~

Calculation of aerostatic guides. Star. 1 inst. 22 no. 9 1964
My '64. (MIRA 17:7)

MAKAROV, V.A.; KOSOTURKIN, Ya.M.; KNYAZHEVA, V.M.; MAMIN, Ye.P.

Range of action of the specific prevention of measles in convalescent
media. Zashch.met. 1 no.0266-009 1-2 1965. (MIRA 58412)

3. Nauchno-issledovatel'skiy Matematicheskii Institut
Imeni I.Ya.Karapova, Moskva.

MAKAROV, V.A.

Division of tuffaceous formation in the Tunguska syneclise.
Izv.vys.ucheb.zav.; geol. i razv. 7 no.3:134-137 Mr '64. (MIRA 18:3)

1. Leningradskiy gornyy institut im. G.V.Flekhanova.

YANCHUK, E.A.; MAKAROV, V.A.

Method of making a photometric wedge for measuring the reflective
power of minerals. Min. sbor. no.17:207-210 '63. (MIRA 17:11)

1. Gosudarstvennyy universitet imeni Franko, L'vov.

TUROVSKIY, S.D.; MAKAROV, V.A.; NOSYREV, I.V.

Find of ore pebbles in Lower Carboniferous conglomerates
of the Boordu region (northern Tien Shan). Dokl. AN SSSR
147 no.1:210-211 N '62. (MIRA 15:11)

1. Institut geologii AN Kirgizskoy SSR. Predstavleno
akademikom D.S. Korzhinskim.
(Boordu region--Ore deposits)

LITVINENKO, O.K.; MAKAROV, V.A.

Using electronic machines to solve a direct problem of gravity prospecting for three-dimensional convex bodies (seismic structures). Prikl. geofiz. no.33:155-160 '62. (MIRA 15:10)
(Gravity prospecting) (Electronic calculating machines)

KURANCHEV, M.I., starshiy nauchnyy sotrudnik; MOISEYEV, I.F.;
MAKAROV, V.A.

Forcing cement mixes behind the lining of railroad tunnels
without stopping the traffic. Transp.stroi. 10 no.8:
19-22 Ag '60. (MIRA 13:8)

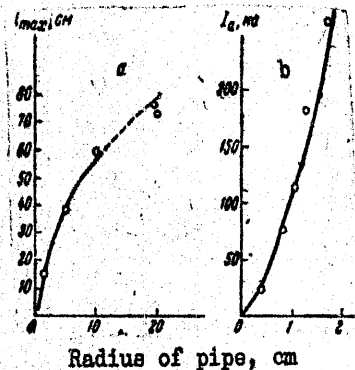
1. Tsentral'nyy nauchno-issledovatel'skiy institut transportno-
go stroitel'stva (for Kuranchev). 2. Nachal'nik tunnel'no-
mostovogo otryada No.1 (for Moiseyev). 3. Nachal'nik
mostopoyezda No.57 (for Makarov).
(Tunnels--Maintenance and repair)

L 23871-66

ACC NR: AP6008/23

equation is solved for various initial and boundary conditions. The calculated results are compared with experimental results of C. Edeleanu and I. Gibson (Cher. Ind., 1961, N. 10, 301) (see Fig. 1).

Fig. 1. Comparison of calculated and experimental data for steel 18-8 in 30% sulfuric acid. a - extent of passive region for the case of partially passivated construction; b - current from the active region of the pipe. Open circles: experimental data taken from reference cited.



It is suggested that the derived expression for the depth of anodic protection should prove useful in the development of methods for the protection of pipelines exposed to the action of corrosive media. Orig. art. has: 5 graphs and 19 equations.

SUB CODE: 07, 13/ SUBM DATE: 19Apr65/ ORIG REF: 007/ OTH REF: 009

Card 2/2 dda

I 23871-66 EWP(m)/EWA(d)/EWP(t)/EWP(k) IJP(c) JD/WB

ACC NR: AP6008/23

SOURCE CODE: UR/0365/65/001/006/0662/0669

AUTHORS: Makarov, V. A.; Kolotyrkin, Ya. M.; Knyazheva, V. M.; Mamin, Ye. B. 52
51ORG: Scientific Research Physico-Chemical Institute im. L. Ya. Karpov (Nauchno-
issledovatel'skiy fiziko-khimicheskiy institut) BTITLE: The extent of anode protection of metals from corrosion in corrosive media

SOURCE: Zashchita metallov, v. 1, no. 6, 1965, 662-669 18

pipeline, steel,

TOPIC TAGS: electrochemistry, corrosion, corrosion protection, corrosion resistant
steel/ 18-8 steel

ABSTRACT: A theoretical derivation for the depth of anodic protection offered to a metal pipe surface exposed to corrosive media is presented. The derivation is based on the assumption that the anodic polarization curve in the region of the "active loop" may be divided into a finite number of regions, for each of which the current-potential relationship may be expressed by an equation similar in form to Tafel's equation. It is also assumed that, in passive region, the current density is independent of the potential. The differential equation

$$\left[\frac{\partial^2 \varphi}{\partial x^2} - \frac{2\rho}{r} f(\varphi) = 0 \right]$$

is derived, where $f(\varphi) = i$, i is the current, φ the potential on the outer surface of the pipe, r is the radius of the pipe, and ℓ the depth of anodic protection. This

Card 1/2

UDC: 620.197.5

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001031500041-6

MAKAROV, V.A., kand.med.nauk

Evaluation of the arterial vascular tonus by the magnitude of
the oscillographic index. Klin. med. 40 no.11:157 N'62
(MIRA 16:12)

ASKEROV, Ali Aslanovich, kand. med. nauk; KOVALEV, Yefim Ivanovich,
kand. med. nauk; MAKAROV, V.A., red.; BASHMAKOV, G.M., tekhn.
red.

[Medical control of physical exercises for elderly subjects]
Vrachebnyi kontrol' pri zaniatiiakh fizicheskimi uprazhneniiami
v starshem vozraste. Moskva, Medgiz, 1962. 180 p.
(MIRA 15:12)

(EXERCISE THERAPY)
(AGED--CARE AND HYGIENE)

MAKAROV, Vladimir Aleksandrovich

[Arterial oscillography in medical supervision of sports]
Arterial'naya ostsillografiia vo vrachebno-sportivnoi praktika,
Moskva, Medgiz, 1958. 66 p. (MIRA 12:2)
(BLOOD PRESSURE)

USSR / Human and Animal Physiology. Blood Circulation.

T-4

Abs Jour : Ref Zhur - Biologiya, No 1, 1959, No. 3422

considerably greater elevation in them after a workload,
to a greater build-up of the systolic volume of the heart
and a lesser tonus of the small arteries. -- V. V.
Rozenblat

Card 3/3

USSR / Human and Animal Physiology. Blood Circulation.

T-4

Abs Jour : Ref Zhur - Biologiya, No 1, 1959, No. 3422

After a dosaged exercise (stationary running), the arterial pressure of the fingers rose to an average of 98.4 mm Hg in the trained and to 84.8 mm Hg in the untrained, the capillary blood circulation became more intensive (especially in the trained athletes). Following a training-exercise, the arterial pressure of the finger rose in the boxers and wrestlers (to an average of 106 - 107 mm Hg in the trained and up to 90 - 91 mm Hg in the untrained) and the number of capillaries in the field of vision increased; in the swimmers, a sinking of the arterial pressure of the finger (down to 65.8 mm Hg in the trained and to 61.1 mm Hg in the untrained) and a spasm of the capillaries was noted, which may be explained by the reflectory effect of the cold water (15 - 23°). The author relates the higher values of the arterial pressure of the finger in the trained at rest, and its

Card 2/3

USSR / Human and Animal Physiology. Blood Circulation.

T-4

Abs Jour : Ref Zhur - Biologiya, No 1, 1959, No. 3422

Author : Makarov, V. A.

Inst : Not given

Title : Variations of the Blood Circulation in Small Arteries
and Capillaries During Sport Exercises

Orig Pub : Teoriya i praktika fiz. kultury, 1957, 20, No 4, 281-285

Abstract : Twenty boxers, 20 wrestlers, and 20 swimmers, ranging in age from 18 - 35 years, were the subject of a study. At rest, arterial pressure readings of the finger, taken by Gaertner's tonometer in combination with the oscillograph of Serkin, were in the average 86.1 mm Hg in trained and 77.3 mm Hg in untrained persons; the capillaroscopic picture of the ungual skin fold was normal in both groups; the number of capillaries in the linear field of vision amounted to 16 in the average.

Card 1/3

MAKAROV, V.A.

Asymmetry in the function of the visual analyzer during muscular work [with summary in English]. Zhur.vys.nerv.deiat. 7 no.3:359-362 My-Je '57. (MIRA 10:10)

1. Kafedra lechebnoy fizkul'tury u vrachebnogo kontrolya Tsentral'nogo instituta usovershenstvovaniya vrachey.

(EXERCISE, effects,

on visual analyzer electrical sensitivity threshold in cerebral cortex (Rus))

(CEREBRAL CORTEX, physiology,

visual analyzer electrical sensitivity threshold in exercise (Rus))

MAKAROV, V.A., kandidat meditsinskikh nauk

Effect of physical stress on arterial tonus in athletes. Sov.med
19 no.6:44-49 Je '55. (MLRA 8:9)

1. Iz kafedry lechebnoy fizkul'tury i vrachebnogo kontrolya
(zav.-prof. V.N. Moshkov) Tsentral'nogo instituta usovershenstvovaniya vrachey (dir. V.P. Lebedeva)

(ATHLETES, physiology,
eff. of effort on arterial tonus in athletes)
(EXERCISE, effects,
on arterial tonus in athletes)
(ARTERIES, physiology,
eff. of effort on tonus in athletes)

MARKOV, V. I.

"Application of Certain Methods of Investigating the Cardiovascular System in Medical Practice in Sports." Izvestiya SSSR, Central Inst for the Advanced Training of Physicians, 16 Feb 54. Dissertation (Izdatyevaya Moskva Moscow, 5 Feb 54)

SO: SUW 136, 19 Aug 1954

MAKAROV, V.A.

25790 Makarov, V.A. O Nekotorykh Voprosakh Organizatsii Meditsinskoy Pomoshchi Invalidam Otechestvennoy Voiny. V Sb: Problemy Vosstanovit. Lecheniya Invalidov Otechestv. Voiny. Astrakhan', 1948, S. 5-11.

SO: Letopis' Zhurnal Statey, No. 30, Moscow, 1948

VINOGRADOV, K.; MAKAROV, V.

Public inspection is mobilizing. Na stroi.Ros. 6 no.2:
19 F '65. (MIRA 19:1)

1. Zamestitel' nachal'nika tekhnicheskogo upravleniya Glavnogo upravleniya po stroitel'stvu v Moskovskom ekonomicheskom rayone Ministerstva stroitel'stva RSFSR (for Vinogradov). 2. Nachal'nik laboratorii kontrolya kachestva Glavnogo upravleniya po stroitel'stvu v Moskovskom ekonomicheskom rayone Ministerstva stroitel'stva RSFSR (for Makarov).

MAKAROV, V., polkovnik

The strength of the press is in party leadership. ~~Komun.~~
Vooruzh. Sil 46 no.6:88-92 Mr '65. (MIRA 18:11)

MAKAROV, V., inzhener-podpolkovnik; ALEKSEYENKO, V., inzhener-kapitan

Checking thermostats. Tekh. i vooruzh. no. 4:24 k '64.
(MIRA 17:6)

MAKAROV, V., kand.tekhn.nauk; PROKHOROVA, A., nauk.tekhn.nauk

Characteristics of the storage of pulse crop seeds. Muk.-slev.
prom. 28 no.9:5-7 S '62. (MIRA 15:10)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut zerna i
produkov yego pererabotki.
(Seeds--Storage) (Legumes)

MAKAROV, V.; PROKHOROVA, A.; PIMANOV, A.

Increasing the volume weight of grain by drying. Muk.-elev. prom.
26 no.9:12-13 S '60. (MIRA 13:9)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut zerna i produktov
yugo pererabotki (for Makarov, Prokhorova). 2. Proizvodstvenno-
tekhnicheskoye upravleniye Goskhlebkomiteta (for Pimanov).
(Grain-- Drying)

PROKHOROVA, A., kand. tekhn. nauk; MAKAROV, V., kand. tekhn. nauk;
GRUVICH, B., kand. tekhn. nauk; PINENOV, A., agro-khimik

Effect of the composition of coal on the quality of dried wheat.
Muk.-elev. prom. 25 no.8:18 Ag '59. (MIRA 13:1)
(Wheat--Drying) (Coal)

ZHDANOV, S., kand.tekhn.nauk; MAKAROV, V., inzh.; KROTOVA, O., inzh.

Device capable of seeing the invisible. Pozh.delo 9 no.7:22-23
Jl '63. (MIRA 16:10)

MAKAROV, V.

Automatic control of the pumping station of the Kirovsk-Omsk Grain Elevator. Muk.-elev. prom. 27 no.7:16-17 Jl '61. (MIRA 14:7)

1. Glavnyy energetik Kirovsk-Omskogo elevatora.
(Pumping stations)

FAYERSHTEYN, V., inzh.; MAKAROV, V., inzh.

Unit for probing soils. Na stroi. Ros. 4 no. 6:12-13 Je '63.
(MIRA 16:6)

(Soils--Testing)

LYUBIMOVA, V.V., doktor ekon. nauk; NOVIKOVA, O.G., kand. ekon. nauk;
 SERGEYEVA, A.G., kand. ekon. nauk; IVANOV, N.P., kand. istor.
 nauk; OBORINA, G.A., kand. ekon. nauk; KHLINOV, V.N., kand.
 ekon. nauk; DANILEVICH, M.V., doktor ekon. nauk; POKATAYEVA,
 T.S., kand. ekon. nauk; USOV, G.A., kand. ist. nauk;
 SAL'KOVSKIY, O.V., kand. geogr. nauk. Prinimali uchastiye:
 PESCHANSKIY, V.V., kand. ist. nauk; PIROGOVA, I.M.; PRONIN,
 S.V.; USVYATSOV, A.Ye.; MAKAROV, V., red.; DARONYAN, M.,
 mladshiy red.; ULANOVA, L., tekhn. red.

[Real wages during the period of the general crisis of capi-
 talism]Real'naya zarabotnaya plata v period obshchego krizisa
 kapitalizma. Moskva, Sotsekgiz, 1962. 558 p. (MIRA 16:3)

1. Akademiya nauk SSSR. Institut mirovoy ekonomiki i mezhdunarodnykh otnosheniy.
 (Wages)

KUZ'MIN, N.A.; MAKAROV, T.V.

Propagation of a quasi-H₀₁ wave in an H-shaped wave guide. Izv. vys.
ucheb.zav.; radiofiz. 6 no.3:581-584 '63. (MIRA 16:2)
(Electromagnetic waves) (Wave guides)

L 17291-63 IDS

ACCESSION NO: AP3004844

S/0141/63/006/003/0581/0584

AUTHOR: Kuz'min, N. A.; Makarov, T. V. 45

TITLE: Propagation of quasi- H_{01} mode in a cross-shaped waveguide

SOURCE: IVUZ. Radiofizika, v. 6, no. 3, 1963, 581-584

TOPIC TAGS: cross-shaped waveguide, waveguide, H_{01} mode

ABSTRACT: This is a continuation of the authors' work (Izv. vyssh. uch. zav. - Radiofizika, 4, 1089, 1961). The Ritz method is again used to find a second approximation to the eigenvalue and eigen function of a quasi- H_{01} mode in a sector-cross waveguide. This data permits determining geometrical parameters of the waveguide which would ensure passing H_{01} mode with a minimum disturbance. Calculated curves serve to determine the optimum, insofar as the "purity" of the H_{01} -mode field is concerned, cross-section of the waveguide. Orig. art. has: 3 figures and 2 formulas.

Card 1/2

Attenuation of electromagnetic ...

34073
S/109/62/007/001/011/027
D266/D301

κ - transverse wave number, k - wave number in free space, S_1 - cross-section of the waveguide, L - boundary of S_1 , $\tilde{\Psi}$ - eigenfunction. Here \tilde{h} , $\tilde{\kappa}$ and $\tilde{\Gamma}$ are unperturbed quantities. The eigenfunctions and eigenvalues of a number of H modes in a rectangular cross shaped waveguide are determined by N.A. Kuz'min and T.V. Makarov (Ref. 2: Radiotekhnika i elektronika, 1961, 6, 12, 1989). The author takes the previously derived eigenfunctions, substitutes them into (1), performs the integration and gives numerical results for the quasi- $(H_{01} + H_{10})$ and quasi- $(H_{02} + H_{20})$ modes. The eigenfunctions for a sectoral cross-shaped waveguide are also determined by Kuz'min and Makarov (Ref. 3: Izv. vuzov MVO SSSR (Radiofizika), 1961 6). Substituting again into (1) the author calculates the attenuation for a quasi- H_{01} wave and concludes that the attenuation of this mode in the cross-shaped waveguide is always larger than that of the H_{01} mode in a circular waveguide. There are 3 figures and 3 Soviet-bloc references.

SUBMITTED: April 13, 1961

Card 2/2

34033

S/109/62/007/001/011/027
D266/D301

9.1300

AUTHOR:

Makarov, T.V.

TITLE:

Attenuation of electromagnetic waves due to losses in
the walls of cross-shaped waveguides

PERIODICAL:

Radiotekhnika i elektronika, v. 7, no. 1, 1962,
99 - 104

TEXT: The purpose of the paper is to calculate the attenuation of certain transverse electric waves in cross-shaped waveguides (both for rectangular and sectoral cross-section). The author starts the analysis by writing up the general formula (derived with the aid of Leontovich boundary conditions) for attenuating H waves in a waveguide of arbitrary cross-section

$$\beta = \frac{w}{2\tilde{h}} \frac{\tilde{h} \oint_L \left| \frac{\partial \tilde{\psi}}{\partial l} \right|^2 dl + \tilde{h}^2 \oint_L |\tilde{\psi}|^2 dl}{k \tilde{h} \iint_{S_\perp} |\tilde{\psi}|^2 dS_\perp}, \quad (1)$$

where w - wave impedance of the metal, \tilde{h} - propagation coefficient,
Card 1/2

50430
S/109/61/006/012/005/020
D266/D305

Electromagnetic waves in ...

where a is the width of the waveguide (see Fig. 1). The eigenvalues resulting from the first and fourth approximations can be seen in Table 1 as a function of $\sigma = b/2a$. If $\sigma \rightarrow 1$ this mode agrees with the sum of the H_{01} and H_{10} modes in the square waveguide. For this reason the author calls this mode a quasi- $(H_{10} + H_{01})$ mode (Fig. 1a)

In a similar manner the properties of a number of other modes are calculated namely quasi- H_{11} (Fig. 1b), quasi- $(H_{20} + H_{02})$ (Fig. 1c), quasi- $(H_{12} + E_{21})$ (Fig. 1d), quasi- H_{22} (Fig. 1e), quasi- $(H_{30} + H_{03})$ (Fig. 1f), quasi- $(H_{40} - H_{04})$ (Fig. 1g), quasi- E_{11} (Fig. 1h), quasi- $(E_{12} + E_{21})$ (Fig. 1i). It is shown that the eigenvalues of the H_{01} and E_{11} modes are different which suggests the possibility of using a cross-shaped waveguide for the bends of an H_{01} transmission system. There are 2 figures, 9 tables and 3 references: 2 Soviet-bloc and 1 non-Soviet-bloc.

SUBMITTED: April 12, 1961

Card 3/8

30430

S/109/61/006/012/005/020
D266/D305

Electromagnetic waves in ...

is minimized. In (1) and (4) $\tilde{\psi}$ and ψ stand for the transverse wave functions of the H and E modes respectively, $\tilde{\kappa}$ and κ are the respective eigenvalues (cut-off wave numbers) of the above modes. The nth approximation of the wave function is written in the following form:

$$u_n = \sum_{i=1}^n a_i \varphi_i \quad (6) \quad 4$$

where the φ_i functions satisfy the boundary conditions and the a_i coefficients are chosen to satisfy the equation system

$$\sum_{i=1}^n a_i [(\nabla \varphi_i, \nabla \varphi_j) - \left\{ \frac{\tilde{\kappa}}{\kappa} \right\}^2 (\varphi_i, \varphi_j)] = 0; \quad j = 1, 2, 3, \dots, n. \quad (7)$$

where the brackets denote scalar multiplication. For the first H mode the trial function is assumed as follows:

$$\tilde{\psi}_1 = a_1 \sin \frac{\pi x}{2a} - a_2 \sin \frac{\pi y}{2a} + a_3 \sin \frac{3\pi x}{2a} - a_4 \sin \frac{3\pi y}{2a}.$$

Card 2/8

30430
S/109/61/006/012/005/020
D200/D305

9,1300

AUTHORS: Kuz'min, N.A., and Makarov, T.V.

TITLE: Electromagnetic waves in rectangular cross-shaped waveguides

PERIODICAL: Radiotekhnika i elektronika, v. o, no. 12, 1961, 1989 - 1997

TEXT: The authors' purpose is to determine the electric and magnetic field configuration for a number of modes in the cross-shaped waveguide. The partial differential equation

$$\Delta \left\{ \begin{matrix} \tilde{\psi} \\ \psi \end{matrix} \right\} + \left\{ \begin{matrix} \tilde{x} \\ x \end{matrix} \right\}^2 \left\{ \begin{matrix} \tilde{\psi} \\ \psi \end{matrix} \right\} = 0 \quad (1)$$

is solved approximately with the aid of the Raleigh-Ritz method, i.e. the integral

$$\left\{ \begin{matrix} \tilde{x} \\ x \end{matrix} \right\}^2 = \iint_{S_{\perp}} \left(\nabla \left\{ \begin{matrix} \tilde{\psi} \\ \psi \end{matrix} \right\} \right)^2 dS_{\perp} \quad (4)$$

Card 1/13

Electromagnetic waves

S/141/61/004/006/012/017
E192/E382

ASSOCIATION

Tsentral'nyy nauchno-issledovatel'skiy
institut svyazi, Moskva (Central Scientific
Research Institute of Communications, Moscow)

SUBMITTED:

April 15, 1961

Card 8/88

3325

Electromagnetic waves

S/141/61/004/006/012/017
E192/E382

$$\psi_1 = \omega(r, \varphi) \left\{ a_0 + \sum_n a_{n+1} J_n(2.405r/a) [\cos(n\varphi) + \sin(n\varphi)] \right\}$$

$$(n = 0, 1, 2, 3, \dots)$$

where $\omega(r, \varphi)$ is a continuous function having finite and continuous derivatives inside the region S_L . The coordinate functions φ_i are also determined for the quasi- E_{11} waves.

The results are illustrated in some graphs and tables from which it is seen that no degeneration takes place between H_{01} and E_{11} waves in a cross-shaped waveguide. It is therefore possible to use such a waveguide for transmitting H_{01} waves in waveguide bends. There are 6 figures, 5 tables and 3 Soviet-bloc references.

Card 7/8

Electromagnetic waves

33225
S/141/61/004/006/012/017
E192/E382

$$\psi_1 = \sum_n a_n J_n(1.84 r/a) [\cos(n\varphi) - \sin(n\varphi)] \quad (n = 1, 2, 3, \dots)$$

On the basis of this equation, a set of graphs is constructed for the eigen value $b\tilde{x}_1$ of the quasi- H_{11} wave as a function of Θ or $\mu = b/a$ (for various values of μ or Θ). This is shown in Fig. 2. Similar solutions are determined for the quasi- H_{21} and H_{01} waves. With regard to the critical frequency of the principal electric wave (quasi- E_{01}), this is determined by calculating the minimum non-zero eigen value of Eq. (1), subject to the conditions of Eq. (3). It is shown that the coordinate functions in this case are composed of a system of functions consisting of a product of function $\omega(r, \varphi)$ and various combinations of trigonometric and Bessel functions

Card 6/88

33225

S/141/61/004/006/012/017
E192/E382

Electromagnetic waves

φ_i (Ref. 1: S.G. Mikhlin: Direct Methods in Mathematical Physics GITTL, M-L, 1950) should satisfy the boundary condition of Eq. (3). A sequence of functions of φ_i should form a complete linearly-independent system. The coefficients a_i are chosen by finding the minimum for Eq. (4) under the condition expressed by Eq. (5). First, the magnetic waves are considered and it is pointed out that the eigen value of Eq. (2) for the condition of Eq. (2) for a cylindrical waveguide is given by the first root of the equation $J_1^0(x) = 0$, which is equal to $1.84/a$, where a is the internal radius of the cylinder. Two degenerate magnetic waves of the H_{11} type correspond to this eigen value in a circular waveguide. The approximate solution of Eq. (6) for the quasi- H_{11} wave in a cross-shaped waveguide of Fig. 1a is therefore assumed to be in the form:

Card 5/8

33225

S/141/61/004/006/012/017
E192/E382

Electromagnetic waves

under the conditions that:

$$\int \int_{S_{\perp}} \left\{ \frac{\tilde{\psi}}{\psi} \right\}^2 dS_{\perp} = 1 \quad (5)$$

where ∇ is the two-dimensional Hamiltonian operator. The eigen values and the eigen functions can be determined by using the Ritz method, according to which the approximate solutions are in the form of a series:

$$u_n = \sum_{i=1}^n a_i \varphi_i \quad (6)$$

where a_i are unknown coefficients. The function

Card 4/88

33225

S/141/61/004/006/012/017
E192/E382

Electromagnetic waves

$$H_z = \tilde{\kappa}^2 \tilde{\psi} ; \quad E_z = \kappa^2 \psi$$

and

$$\begin{pmatrix} \tilde{\kappa} \\ \kappa \end{pmatrix} = k^2 = \begin{pmatrix} \tilde{h} \\ h \end{pmatrix}^2$$

where \tilde{h} and h are propagation constants of the magnetic and electric waves, respectively. It is known that the extremum functionals, whose Euler equations are in the form of Eqs. (1), are in the form:

$$\begin{pmatrix} \tilde{\kappa} \\ \kappa \end{pmatrix}^2 = \int_{S_{\perp}} \left(\nabla \begin{pmatrix} \tilde{\psi} \\ \psi \end{pmatrix} \right)^2 dS_{\perp} \quad (4)$$

Card 3/8

Electromagnetic waves

33225
S/141/61/004/006/012/017
E192/E382

a) for magnetic waves -

$$\partial \tilde{\psi} / \partial n|_L = 0 \quad (2)$$

b) for electric waves -

$$\psi|_L = 0 \quad (3)$$

These boundary conditions apply on the contour L of the transverse cross-section S_\perp of the waveguide. The operator Δ in Eq. (1) is the two-dimensional Laplace operator, ϵ and μ are eigen values of magnetic and electric waves respectively; \underline{n} is the external normal to the contour. The functions $\tilde{\psi}$ and ψ are the longitudinal components of the magnetic and electric Hertz vectors, which are related to the longitudinal field components by the following equations

Card 2/18

9.1300

33225
S/141/61/004/006/012/017
E192/E382

AUTHORS: Kuz'min, N.A. and Makarov, T.V.

TITLE: Electromagnetic waves in a cross-shaped waveguide consisting of a number of sectors

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Radiofizika, v. 4, no. 6, 1089 - 1098, 1961

TEXT: The system considered is illustrated in Fig. 1a, where the relevant geometrical parameters are indicated. Determination of fields and critical frequencies of the electromagnetic waves of E- and H-types in a regular ideally-conducting waveguide (such as shown in Fig. 1) is based on the solution of the scalar equations of the type:

$$\Delta \begin{pmatrix} \psi \\ \psi \end{pmatrix} + \begin{pmatrix} \kappa \\ \kappa \end{pmatrix}^2 \begin{pmatrix} \psi \\ \psi \end{pmatrix} = 0 \quad (1)$$

with the following boundary conditions:

Card 1/8. 8

MAKAROV, T.A., Inzh. (Ust'-Kamenogorsk)

Improvement of boiler protection networks. Energetik 13 no.5:
23-24 My '65. (PML 13:3)

NAKABOV, S. Z.

Chemistry

DECEASED
c. 1961

see ILC

1962
/7

ANAN'YEV, Ivan Vasil'yevich; TIMOFEYEV, Pavel Grigor'yevich.
Prinimala uchastiye UL'YANOVA, Yu.T.; MAKAROV, S.Ya.,
inzh., retsenzent; ZASLAVSKIY, B.V., kand. tekhn.
nauk, red.; BURAKOVA, O.N., red.

[Vibrations of elastic systems in airplane structures
and their damping] Kolebaniia uprugikh sistem v aviatsion-
nykh konstruktsiyakh i ikh dempfirovaniye. Moskva, Mashino-
stroenie, 1965. 525 p. (MIRA 18:4)

MAKSIMOV, V., podpolkovnik, kand.voyennykh nauk; ORESHCHENKOV, A., kapitan;
MAKAROV, S., starshiy inzhener-leytenant; GOLOVIN, P., inzhener-
podpolkovnik

What do you suggest? Av.1 kosm. 45 no.8:70-71 '62. (MIRA 15:8)
(Aeronautics, Military)

SHEYNIN, Viktor Mikhaylovich; YAGODIN, Ye.I., inzhener, retsenzent;
MAKAROV, S.Ya., inzhener, retsenzent; ZAYTSEVA, K.Ya., inzhener,
nauchnyy redaktor; PETROVA, I.A., izdatel'skiy redaktor;
CHISTYAKOVA, A.V., tekhnicheskii redaktor

[Calculating aircraft centering] Raschet tsentrovki samoleta.
Moskva, Gos. izd-vo obr.promyshl., 1955. 226 p. (MIRA 9:8)
(Airplanes--Design and construction)

Spravochnaya kniga po raschetu samoleta na prochnost'

AID 510 - I

- Facilities: None
- No. of Russian and Slavic References: 14 before 1939, 38 after this date. A number of footnotes are given in parts 4 and 5.
- Available: A.I.D., Library of Congress.

Spravochnaya kniga po raschetu samoleta na prochnost'	AID 510 - I
Ch. V Semi-Monocoque Fuselage	544-564
Local stresses in the skin; Conical casing; Frames; Lighting holes and flanges; General losses of stability of semi-monocoque fuselages	
Ch. VI Truss Fuselage	565-573
Practical hints; Symmetrical loading; Torsion; Lateral loading.	
Ch. VII Landing Gear	574-584
Ch. VIII Engine Mount. In-line and Radial Engines	585-601
Ch. IX Empennages, Ailerons, Flaps and Controls	602-643
Forces in the empennage; Reaction in elastic supports of the wheel (determination by energy considerations); Diagrams for the determination of the stabilizer; Special features of swept back empennage; Special features of the wheel with a Vee shaped rotation axis; Details of the empennage; Wheels; Ailerons; Simple and split flaps; Controls.	
PART SIX SHOCK ABSORBERS, LANDING GEAR. PRINCIPAL SYMBOLS	
Ch. I. Landing Gear Shock Absorbing	644-659
Shock absorbing operation; Diagrams of pressing and the work of a shock absorber; Characteristics and choice of pneumatics.	
Ch. II Oleo-Pneumatics. Design, Checking	660-690
Ch. III Rubber Shock Absorbers	691-696
Appendix Joints	697-700
Purpose: This book is intended for engineers and designers; it may be useful also to students of aviation institutes of higher learning.	

Spravochnaya kniga po raschetu samoleta na prochnost'

AID 510 - I

of frames taking account of elasticity; Calculation of wooden spars for bending

PART FOUR CALCULATION OF PLATES

Ch. I Flat Isotropic Plate 411-420

Compression; Eccentric compression and bending; Compression from all four sides; Shearing; Simultaneous action of compression and bending; Oblique-angled plates.

Ch. II Curved Isotropic Plate 421-432

Compression; Shearing; Torsion; Compression and shearing.

Ch. III Bending of Tubes 433-434

Ch. IV Calculation of Plates for Normal Pressure 435-456

Flat rectangular Plates; Curvilinear plates; Spherical plates; Plates with filler.

PART FIVE AIRCRAFT DESIGN CALCULATIONS

Ch. I Monocoque Wings 457-499

Geometric data on wing sections; Linear loads; Torsional axes of the wing; Moments, secant and axial forces; Normal stresses; Tangent stresses due to bending; Tangent stresses due to torsion; Secondary normal stresses due to bending; Tangent stresses due to torsion in fixed points; Deflexions and angles of torsion; Partition ribs; Plastic deformations.

Ch. II Semi-Monocoque Wings 500-531

Secondary, normal and tangent stresses due to bending; Reduction coefficients in tensile and compressed areas; Shear in walls.

Ch. III Braced Wing 532-537

Ch. IV Special Features of Swept Back Wings 538-543

Spravochnaya kniga po raschetu samoleta na prochnost'

AID 510 - I

thin-walled sections; Center of rigidity of open sections; Closed sections, Position of the center of rigidity of various sections; Bending work of a section with flanges and non-working walls; Distribution of tangential stresses in shearing for some sections.	286-306
Ch. VII Combined Bending and Axial Stress Combined bending and axial stresses in struts of uniform section; Combined bending and axial stresses in tubes; Combined bending and axial stresses in hinged bars of variable sections; Short struts of variable sections; Combined bending and axial stresses in bars with excentricity of axial force.	XXXXXX 307-319
Ch. VIII Trusses XXXXXX Statically determinate and indeterminate trusses	320-342
Ch. IX Frames Methods of calculation of frames; Formulae for calculation of simple frames	343-347
Ch. X Curved Beams Stresses and deformations; Formulae; Bending	348-366
Ch. XI Arches Arches with two and three hinges; Arches with fixed Abutments; Arches with greater rise; Stability of arches.	367-373
Ch. XII Springs	374-406
Ch. XIII Rings and Frames Formulae for the calculation: of bars of uniform section curved according to an arc of a circle, of circular rings, of oval rings (frames) of constant section; Graphs for the determination of stresses in circular rings (frames) of constant section; Graphs for the calculation	

Spravochnaya kniga po raschetu samoleta na prochnost'	AID 510 - I
Ch. III Semi-finished Products and Structural Elements	143-163
Wires, cables, bands, tenders; Ball bearings; Springs; Graphics for the calculation of lugs; Rivets; Tubular rivets and solid bolts; Welding; Spring locks and screws with riveted nuts.	
PART THREE CONSTRUCTION MECHANICS	
Ch. I Tension and Compression	164-167
Basic formulae of tension and compression; Effect of orifices and scorches; Effect of the direction of rolling.	
Ch. II Crushing	168-171
Basic conceptions. Crushing of metals; Crushing of wood under bolts	
Ch. III Shear	172-173
The diagram and the work of deformation; Admissible stresses of shear.	
Ch. IV Torsion	174-187
Closed thin walled sections; Effect of orifices and scorches on torsional strength; Calculated stresses and the coefficient of plasticity in torsion; Moments of inertia and stresses in torsion of multi sectional bars.	
Ch. V Bending	188-261
Coefficient of plasticity in bending; Formulae for the calculation of beams for bending; Transversal bending with axial loading; Graphic calculation of compressed and bent beams; Multispan beams; Checking of the strength of tubes under combined stresses; Diagonal bending.	
Ch. VI Shear in Bending and Center of Rigidity	262-285
Center of rigidity; Determination of the center of rigidity of	

Spravochnaya kniga po raschetu samoleta na prochnost'

AID 510 - I

unknown in the USA methods of calculation. The novelty of it consists of the compilation of methods of strength calculation which otherwise must be looked for in various handbooks, textbooks and technical periodicals.

Table of Contents

Pages

PART ONE

TABLES AND CALCULATING DATA

Ch. I Measurements

5-9

Correlation between Anglo-American and metric measurements and between some metric measurements; Some gas constants; Speed of sound on various altitudes.

Ch. II Mathematical Tables and Formulae

9-60

Ch. III Geometric Characteristics of Sections

61-113

Comparative data of sections; Calculating data on annular tubes; Calculating data on streamlined tubes; Comparative table of characteristics of corrugation; Coefficient of surface, of moments of inertia and of moments of resistance of some sections.

PART TWO

CHARACTERISTICS OF MATERIALS AND SEMI-FINISHED PRODUCTS USED IN AIRCRAFT CONSTRUCTION

Ch. I General Conceptions of the Characteristics of Materials

114-117

Basic properties; Stress-strain diagrams.

Ch. II Characteristics of Materials

118-142

Symbols and dimensions; Ratio of limit stresses of some metals; Steel; Aluminum alloys; Magnesium alloys; Bronses; Wooden materials; Plastic materials; Aircraft fabrics; Solders easy melting materials; Rubber materials; Glues; The influence of temperature on mechanical properties; Some physical properties of materials; Coefficients of friction.

MAKAROV, S. Ya.

PHASE I

TREASURE ISLAND BIBLIOGRAPHICAL REPORT

AID 510 - I

BOOK

Call No.: AF 641131

Authors: ASTAKHOV, M. F., KARAVAYEV, A. V., MAKAROV, S. Ya., and SUZDAL'TSEV, Ya. Ya.

Full Title: HANDBOOK OF AIRCRAFT STRENGTH CALCULATIONS

Transliterated Title: Spravochnaya kniga po raschetu samoleta na prochnost'

PUBLISHING DATA

Originating Agency: None

Publishing House: State Publishing House of the Defense Industry (Oborongiz)

Date: 1954

No. pp.: 708

No. of copies: NOT given

Editorial Staff: The authors express thanks for help to the following: Shishkin, S. N.,
Doc. of Tech. Sci., Cheremuzhin, A. M., Prof., Doc. of Tech. Sci., Dubrovin, A. A.,
Kand. of Tech. Sci., Kurguzov, D. N., Eng., and Belous, A. A.

TEXT DATA

Coverage: This book is concerned exclusively with statics and does not contain problems not yet thoroughly verified in practice. The general character of the composition is entirely subordinated to the needs of engineers who start working in the field of aircraft strength calculations. Wherever it was possible, formulae were reduced through transformations or graphical interpretations to their practical form. Chapters in which new problems are considered contain more details than it should be expected from a handbook. The book contains, especially in parts 4 & 5, a comparatively large number of American and other foreign references, diagrams, graphs, tables, formulae.

On the basis of a general examination it may be stated that the book does not contain

MAKAROV, S. YA.

O priblizhennom opredelenii poletnogo vesa samoleta i ego chastei.
(Tekhnika vozdushnogo flota, 1945, no. 4, p. 8-10, 22, tables.)

Title tr.: Estimate of gross weight of an aircraft and its components.

TL504.Th 1945

SO: Aeronautical Sciences and Aviation in the Soviet Union, Library of Congress, 1955.

MAKAROV, S. YA.

Mozhno li oblegchit' istrebitel'. (Tekhnika vozdushnogo flota, 1943, no. 3, p. 5-9, tables, diags.)

Title tr.: Is it possible to reduce the weight of a fighter?

TL504.T4 1943

SO: Aeronautical Sciences and Aviation in the Soviet Union, Library of Congress, 1955.

MAKAROV, S.V., assistant

Clinical observations on the use of some therapeutic pastes
in the treatment of deep caries. Vop. obshchei stom. 17:27-
29 '64.

Methodology for the study of the morphological reaction of
the pulp of the carious tooth to the effect of therapeutic
pastes. Ibid.:35-36 (MIRA 18:11)

MAN'KOVSKAYA, N.K.; PONOMARENKO, I. Ya.; UDOVENKO, S.A.; MAKAROV, S.V.;
KHLUD, M.L.

New method for separating and dividing synthetic fatty acids
into fractions. Khim. i tekhn. topl. i masel 9 no.6:52-57
Je'64 (MIRA 17:7)

1. UkrNIIgiproneft' i Vsesoyuznyy nauchno-issledovatel'skiy
i proyektnyy institut sinteticheskikh zhirozameniteley.

MEKAROV, S.V.

Topological evaluation of the memory capacity of a multitest system.
Prohl. pered. inform. 1 no.2:108-111 '65. (MIRA 18:7)

L 5055-66
 ACCESSION NR: AP5024538

orthogonal-nonrepetitive forms. However, there exist difficulties connected with the chopping algorithm due to the number of ONF terms contained in a particular Boolean function. To estimate the complexity of such an algorithm the present author calculates the mathematical expectation E of the number of terms M in the ONF version of the original function. Extended calculations presented in this paper lead to the result

$$E(M) \approx 0.235 \cdot 2^n$$

with a relative error not exceeding 0.001. The article concludes with an application of the chopping algorithm to monotonic functions. Orig. art. has: 57 formulas, 3 figures, and 2 tables.

ASSOCIATION: none

SUBMITTED: 18Jan65

ENCL: 00

SUB CODE: DP, MA

NO REF SOV: 008

OTHER: 000

Card 2/2 *MD*

L 5055-66 EWT(d)/T IJP(c)

ACCESSION NR: AP5024538

UR/0378/65/000/004/0031/0037
512.932

46
B

AUTHOR: Makarov, S. V.

TITLE: Complexity estimate of the chopping algorithm

SOURCE: Kibernetika, no. 4, 1965, 31-37

16.4455

TOPIC TAGS: cybernetics, finite automaton, Boolean function, algorithm, probability

ABSTRACT: In a study of the structural reliability of finite automata and of some other continuously acting devices the problem of finding the probability for the transformation of the Boolean function $f(X_1, \dots, X_n)$ into unity is often encountered. Here all the arguments of the function are random quantities with a known probability distribution. For the solution of this problem the author proposed earlier the so-called "chopping algorithm" (Vychislitel'nyye sistemy, no. 4, Novosibirsk, 1962) which essentially takes the original Boolean function in its orthogonal-nonrepetitive form (ONF) and for each term of this form finds the probability of its conversion into unity. Subsequently, these separate probabilities are combined into the solution of the entire problem. The simplicity of all the necessary calculations is determined basically by the properties of the

Card 1/2

07010182

MAN'KOVSKAYA, N.K.; UDOVENKO, S.A.; MAKAROV, S.V.

Synthetic fatty acids obtained with the method of soap
decomposition by carbonic acid. Khim. i tekhn. topl. i masel 9
no.1:23-26 Ja '64. (MIRA 17:3)

14-00000
ACCESSION NO: ARMO14011

conjunctions, disjunctions and negations. The proper operating condition of an element is designated by one, the improper condition by zero, and methods of probability calculation of single-cycle layouts are then employed. A relationship is established between local (probabilities of proper operation of elements during some cycle) and integral (i.e., the average frequency of failure λ) characteristics of reliability. The proposed procedure makes it possible to obtain quantitative evaluations of the structural reliability of a marine power plant at various operating conditions in relation to different functionally equivalent programs. The program presenting optimum reliability is then selected. G. Yakobson

SUB CODE: PR, MA ENCL: 00

5

CLASS: INT (U) IUP(c)
ACCESSION NO: ARES014011

UR/0872/05/000/004/V025/V025
519, 2:02

SOURCE: *Rel. zh. Kibernetika. Svochny tom, Abs. 4V136*

10
B

AUTHORS: Mokranov, V. A., Maharov, S. V., Ostrov, V. A., Filatov, A. V.

TITLE: A logically-probabilistic method of calculating the reliability of marine power plants

16

ORIG SOURCE: *Sp. Vychisl. sistemy. Vyp. 13. Novosibirsk, 1964, 45-57*

TOPIC TAGS: marine power plant, reliability analysis, logically probabilistic procedure, functionally equivalent program

TRANSLATION: The complexity of calculating the reliability of marine power plants operating under variable loads is attributable to the impracticality of representing a marine power plant layout in the form of a combination of successively-parallel couplings of its elements. The authors propose the use of a logically-probabilistic method employed in analysis of computer programs. The functional interrelation of elements of a marine power plant is written in the form of an equivalent logical program consisting of

Card 1/2